

CE 342 - Fall 2002 - Exam #3
 Problem 2 - Solution
 RJN 12/3/2

Release the moment at d

Calculate the rotation at d due to the thermal gradients in the members.
 Apply a unit couple at d, calculate the reactions and draw the moment diagrams.

Reactions



Moment diagrams for the virtual load



The virtual work equation for displacements (rotations) due to thermal gradients is

$$\theta_d \Delta T \cdot 1 \cdot \text{kip} \cdot \text{in} = \int_a^b \frac{-\alpha \cdot \Delta T}{h} \cdot M_v dx + \int_d^c \frac{-\alpha \cdot \Delta T}{h} \cdot M_v dx$$

If the local coordinates for ab go from a to b, the temperature gradient is positive.

$\Delta T_{ab} := 150 \cdot R - (-20 \cdot R)$ Mathcad uses absolute temperature (Rankine scale) instead of Fahrenheit.
 Since we only care about change in temperature, this isn't a problem.

and M_v is positive.

If the local coordinates for dc go from d to c, the temperature gradient is negative.

$\Delta T_{dc} := -20 \cdot R - 150 \cdot R$

and M_v is negative.

Using the product integral table

$$\theta_{d\Delta T} \cdot 1 \cdot \text{kip} \cdot \text{in} = \frac{L_{ab}}{2} \cdot 1 \cdot \text{kip} \cdot \text{in} \cdot \frac{-\alpha \cdot \Delta T_{ab}}{h_{ab}} + \frac{L_{dc}}{2} \cdot (-1 \cdot \text{kip} \cdot \text{in}) \cdot \frac{-\alpha \cdot \Delta T_{dc}}{h_{dc}}$$

The problem statement gives us

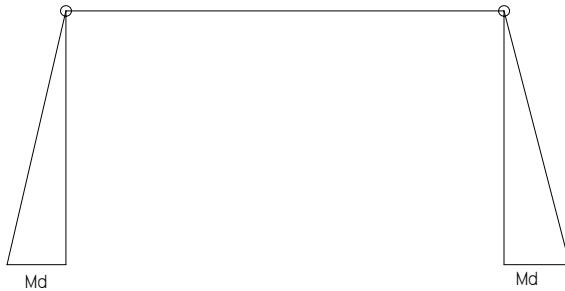
$$\alpha := \frac{6.5 \cdot 10^{-6}}{R} \quad \text{kip} := 1000 \cdot \text{lbf} \quad h_{ab} := 12 \cdot \text{in} \quad h_{dc} := h_{ab} \quad L_{ab} := 20 \cdot \text{ft} \quad L_{dc} := L_{ab}$$

$$E := 29000 \cdot \frac{\text{kip}}{\text{in}^2} \quad I_{ab} := 500 \cdot \text{in}^4 \quad I_{dc} := I_{ab}$$

$$\theta_{d\Delta T} := \left[\frac{L_{ab}}{2} \cdot 1 \cdot \text{kip} \cdot \text{in} \cdot \frac{-\alpha \cdot \Delta T_{ab}}{h_{ab}} + \frac{L_{dc}}{2} \cdot (-1 \cdot \text{kip} \cdot \text{in}) \cdot \frac{-\alpha \cdot \Delta T_{dc}}{h_{dc}} \right] \cdot \frac{1}{1 \cdot \text{kip} \cdot \text{in}} \quad \theta_{d\Delta T} = -0.022 \text{ rad}$$

Calculate the rotation due to the redundant moment M_d .

The moment diagrams for M_d can be scaled from the moment diagram for the unit moment.



and the virtual work equation becomes

$$\theta_{dM_d} \cdot 1 \cdot \text{kip} \cdot \text{in} = \int_a^b \frac{M \cdot M_v}{E \cdot I} dx + \int_d^c \frac{M \cdot M_v}{E \cdot I} dx$$

Using product integrals

$$\theta_{dM_d} = \frac{1}{1 \cdot \text{kip} \cdot \text{in}} \left[\frac{L_{ab}}{3} \cdot \frac{M_d \cdot 1 \cdot \text{kip} \cdot \text{in}}{E \cdot I_{ab}} + \frac{L_{dc}}{3} \cdot \frac{-M_d}{E \cdot I_{dc}} \cdot (-1 \cdot \text{kip} \cdot \text{in}) \right]$$

The compatibility equation is

$$\theta_{d\Delta T} + \theta_{dM_d} = 0$$

Substituting

$$\theta_{d\Delta T} + \left(\frac{L_{ab}}{3} \cdot \frac{M_d}{E \cdot I_{ab}} + \frac{L_{dc}}{3} \cdot \frac{M_d}{E \cdot I_{dc}} \right) = 0$$

$$M_d := -3 \cdot \frac{\theta_{d\Delta T}}{L_{ab} \cdot I_{dc} + L_{dc} \cdot I_{ab}} \cdot E \cdot I_{ab} \cdot I_{dc} \quad M_d = 166.901 \text{ kip} \cdot \text{ft}$$

Scaling the reactions from the unit load case:

$$d_x := \frac{M_d}{240 \cdot \text{in}} \quad d_x = 8.345 \text{ kip}$$

Alternate solution - release the horizontal reaction in the pin at c. Since bc is now essentially simply supported, we can show that there is no shear in bc, only axial forces. Calculate the relative displacement at c due to the thermal forces. Apply an internal horizontal force at c. The moment diagrams are triangular (similar to the previous solution) with a maximum moment of 240 kip inches at a and d. Therefore the thermal displacements are

$$\delta_{d\Delta T} := \left[\frac{L_{ab}}{2} \cdot 240 \cdot \text{kip} \cdot \text{in} \cdot \frac{-\alpha \cdot \Delta T_{ab}}{h_{ab}} + \frac{L_{dc}}{2} \cdot (-240 \cdot \text{kip} \cdot \text{in}) \cdot \frac{-\alpha \cdot \Delta T_{dc}}{h_{dc}} \right] \cdot \frac{1}{1 \cdot \text{kip}} \quad \delta_{d\Delta T} = -5.304 \text{ in}$$

The relative displacement due to the redundant force can be found from beam tables.

$$\delta_{cx} = 2 \cdot \frac{c_x \cdot L_{ab}^3}{3 \cdot E \cdot I_{ab}}$$

Since the relative displacement is zero

$$\delta_{d\Delta T} + \delta_{cx} = 0$$

or

$$\delta_{d\Delta T} + 2 \cdot \frac{c_x \cdot L_{ab}^3}{3 \cdot E \cdot I_{ab}} = 0$$

solving for c_x .

$$c_x := \frac{-3}{2} \cdot \frac{\delta_{d\Delta T}}{L_{ab}^3} \cdot E \cdot I_{ab} \quad c_x = 8.345 \text{ kip}$$

and

$$M_d := c_x \cdot L_{ab} \quad M_d = 166.901 \text{ kip} \cdot \text{ft}$$

Risa stuff

$$M := \frac{\alpha \cdot \Delta T_{ab} \cdot E \cdot I_{ab}}{h_{ab}} \quad M = 111.267 \text{ kip} \cdot \text{ft}$$

$$M + 55.6 \cdot \text{kip} \cdot \text{ft} = 166.867 \text{ kip} \cdot \text{ft}$$